Full scale test results of the RIMOB Crash Cushion

Description of tests and results conform standard CEN/TC 226/WG1

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Preface

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In 1981 and 1982 SWOV has carried out final tests with the RIMOB crash cushion. In those years there were no test conditions for crash cushion available. In accordance with some of the experiences carried out in the United States, chosen is for relevant tests: central impacts, frontal off set impacts and side impacts.

In this report the 'old' tests and results are redescribed similar to standard CEN/TC 226/WG1. Owing to differences between RIMOB and CEN test conditions the given results are not directly comparable. On the other hand there is much agreement.

The RIMOB is developed for passenger car with is a mass of approximately 900 kg. An integrated buffer segment provides for well function to vehicles with a higher mass. Collisions with vehicles with a lower mass give higher values for the Acceleration Severity Index (ASIcriterium) as described in this report.

After the tests the RIMOB is applied in practice. After seven years about 170 impact attenuators have been installed on the medians and shoulders of motorways in the Netherlands. At that time an evaluation study has been carried out (Schoon, 1990). Analyzed are 38 accidents registered by police. From the accident figures it was concluded that the RIMOB functions effectively. Even though collision speeds have been found of over 100 km/h no fatal accident was registered. Of the 38 collisions six resulted in injuries, of which one or two were taken to hospital and four or five only were slight injuries.

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1. Testing laboratory

TNO Wegtransportmiddelen (TNO Road-vehicles Research Institute) Schoemakerstraat 97 P. O. Box 6033 2600 JA DELFT The Netherlands Phone: +31 (0)15 - 696900 Fax: +31 (0)15 - 620766 Test site location: same location as address above

2. Client

Stichting Wetenschappelijk Onderzoek Verkeersveiligheid SWOV (SWOV Institute for Road Safety Research) Duindoorn 32 P. O. Box 170 2260 AD LEIDSCHENDAM The Netherlands Phone: +31 (0)70 - 3209323 Fax: +31 (0)70 - 3201261

Rijkswaterstaat Adviesdienst voor Verkeer en Vervoer AVV (Ministry of transport AVV Consultant for Traffic and Transportation) P. O. Box 1031 3000 BA ROTTERDAM Phone: +31 (0)10 - 4026200

3. Tests with the RIMOB

3.1. Name of road restraint system

Crash Cushion: RIMOB Dutch: RIMpelbuis Obstakel Beveiliger English: Impact attenuator equipted with crumpling tubes.

3.2. Testing dates

F 4, F 5	:27th May	1981
F 6, F 7	:24th June	1981
F 8, F 9	:26th August	1981
F 10	:17th November	1981
F 11, F 12	:18th November	1981
F 13	:27th January	1982

3.3. Description of the RIMOB

A RIMOB (see Annex 1) consists of a composition of box-like segments which are compressed in a head-on collision. Each segment is one metre long and contains aluminium tubes which are placed in axial direction. The tubes serve to be compressed in a violent head-on collision to a maximum of approximately 20% of their initial length. The RIMOB also has side protection that consists of 2 m long guide-rail-elements which are partly placed on top of each other. Because of this placement the parts can slip on top of each other when this is needed. A standard profile is used. In case of a collision with the side of a RIMOB, it functions like a regular barrier construction.

The impact which RIMOB can absorb can be programmed. The absorption can be adjusted by changing the number of segments, the number of crumpling tubes per segment, the diameter of the tubes and the thickness of the tube-walls. The RIMOB is attached to the ground at only two points. The advantages are simple foundation and easy erection. Standard barriers can be connected to RIMOB, so it can be fully integrated.

Two types of RIMOB have been tested: The RIMOB-V 270 and the RIMOB-P 110. The RIMOB-V 270 (see Annex 2) has a V-shape with a base width of 2.70 m. The RIMOB-P 110 (see Annex 3) has a parallel shape with a base width of 1.10 m. The RIMOB-P is developed for a maximum collision speed of 70 km/h.

3.4. Drawing of the RIMOB-types

RIMOB-V (V 270): Annex 1 and 2 RIMOB-P (P 110): Annex 3

4. General test data (tests F4 to F13)

4.1. Vehicles

Opel Kadett-B sedan cars have been used for the crash tests in all cases with exception of test F7 where a Coupé is used.

Vehicle data:

mass:	715 kg to 847 kg
width:	1.57 m
lenght:	4.11 m (coupé: 4.18 m)
wheelbase:	2.42 m
track width:	front: 1.25 m; rear: 1.28 m

Center of gravity:

horizontal distance (x) from front axle: 1.20 m longitudal distance (y) is in the center of the car vertical distance (z) from ground: 0.57 m

4.2. Dummies

In each test vehicle two 'Hybrid II'-dummies were installed. One dummy on the driver-seat and one on the passenger-seat, both wearing safety-belts. The mass of each Hybrid II dummy is 75 kg.

4.3. Data registration

The test vehicles were provided with triaxial acceleration meters, excluded the tests F11 and F13 (see the remark at these tests). For the positions of the acceleration meters see Annex 4.

Apart from acceleration meters, in tests F10 and F12 both dummies were equipted with triaxial acceleration meters; one in the head and the other in the chest. Also shoulder belt loads were registered with Lebow 3419 meters.

4.4. Total weight

In order to prevent fire, the fueltanks were all emptied. To simulate the mass of a full tank, a weight with a mass of 40 kg was added. The weight of the electronic equipment on board is also included.

4.5. Wheather conditions

In all cases it was dry.

5. Test procedure of RIMOB with results

In order to test the RIMOB-V, nine chrash tests were performed. The tests were divided in 4 categories:

- Frontal: 3 tests

- Offset: 2 tests

- 15° Frontal: 1 test

- Side impact 65 km/h - 22° : 1 test

- Side impact 80 km/h - 15°: 2 tests

Most of the impact conditions have been in accordance with the CEN standard. In case of differences the extent is expressed in percents.

With the RIMOB-P one frontal test is carried out.

From each test the impact conditions and results are given. Pre test and post test situations are shown in figures. The acceleration values (horizontal, lateral and vertical) are expressed in the value of the ASI.

In the paragraphs 3.3. 'Injury assessment', the ASI values are given according to CEN standard as well as according to SWOV calculations (resp. mentioned ASI-CEN and ASI-SWOV).

ASI-CEN: the reference acceleration values in the CEN standard are: $a_{hor} = 12g$, $a_{lat} = 9g$ and $a_{vert} = 10g$. With these values the ASI criterium is '1' for belted occupants.

ASI-SWOV: in 1982 SWOV used the reference acceleration values $a_{hor} = 7g$, $a_{tat} = 5g$ and $a_{vert} = 6g$. With these values the ASI criteria is '1' for unbelted occupants and '1.6' for belted occupants. The given time-history curves of ASI values are the ASI-SWOV values.

The ASI criterium is not fully appropriate for side impact tests. See for instance the remarks given at side impact tests F10.

The last page of each test contents pictures of the RIMOB and test vehicle after the test.

In Chapter 6 the final results are given in accordance with in the CEN standard mentioned 'Acceptance Classes'.

5.1. Frontal tests

A. CEN test specifications TC 1.1.C.

Target impact speed:	100 km/h
Target impact angle:	0°
Target impact point:	center
Target vehicle test mass:	900 kg

B. Test performed

Three tests are carried Test impact speed: Test impact angle: Test impact point:	100 km/h (0	: F7, F11 0% differ 0% differ	ence)	
- Test-number:	F7		F11	F13
- Car:	Opel Kadett O 1500 Coupé	Iympia	Opel Kadett B	Opel Kadett B
- Model year:	1970		1973	1971
- Test mass:	997 kg		975 kg	approx. 970 kg
- Test date:	06.24.82 (mm.d	d.yy)	11.18.81	01.27.82

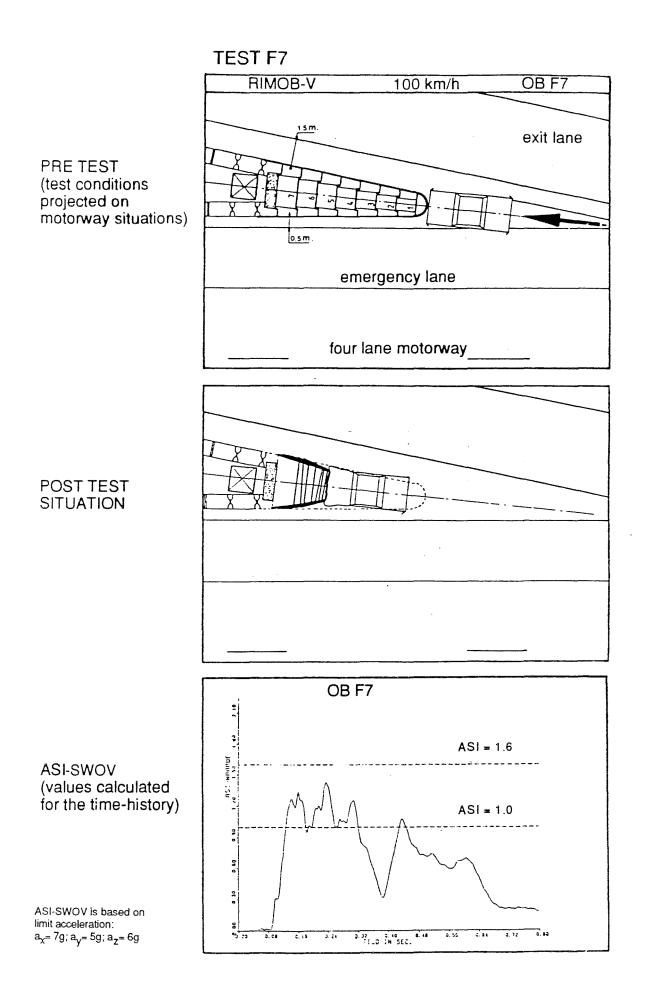
C. Results TC 1.1.C.

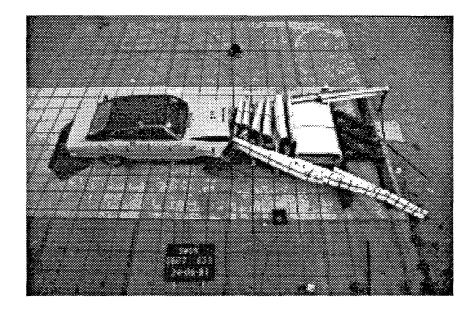
C.1. Data of the RIMOB

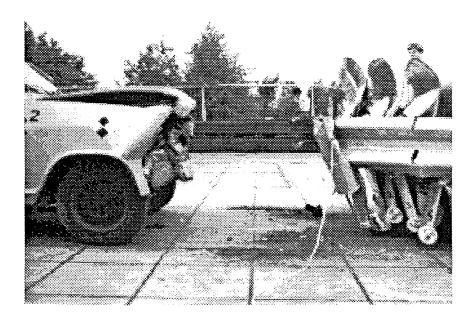
-	Test-	num	ber
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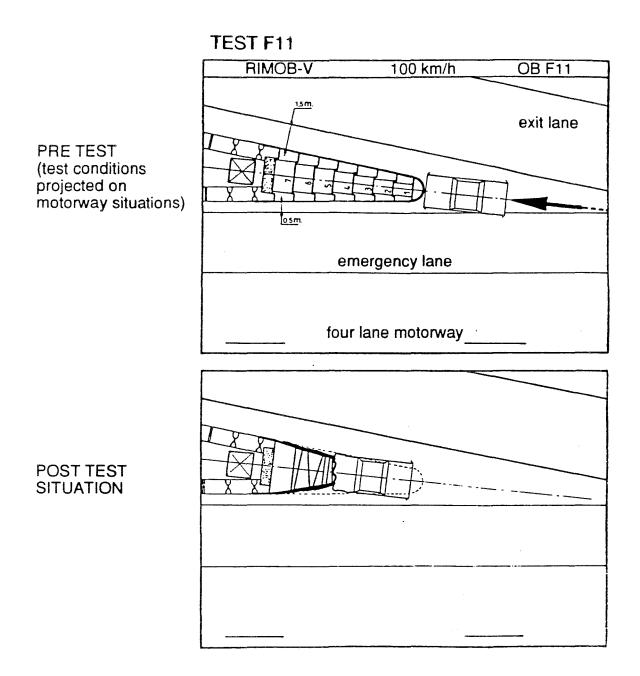
- 1est-number	F7	F11	F13
- Damage to RIMOB:			
	compression: 5.1 m dynamic compression: 5.35 m	compression: 4.5 m dynamic compression: 4.9 m	compression: 4.1 m dynamic compression: 4.9 m
- Maximum permanent d	deflection (lateral):		
	0.1 m	0 m	0 m
- Major parts fractured	or detached?:		
	none	none	none
C.2. Vehicle			
- Rebound:	0	0	A F
	0 m	0 m	0.7 m
- Length reduction of ho		0.26	0.24
	0.25 m	0.26 m	0.34 m
- Vehicle cockpit deformation index VCDI:			
	no deformation	no deformation	no deformation
C.3. Injury assessment			
- Acceleration severity in			
(criteria: $ASI_{max-belied} = 1$)	,0) 0.87	no data *)	no data *)
	ndex ASI-SWOV (zie grap	hs)	
(criteria: $ASI_{max-belied} = 1$,	$\begin{array}{l} 6; \ ASI_{max-unbelled} = 1,0; \\ 1.5 \end{array}$	no data *)	no data *)
- Average acceleration $(a_{avg.} = v^2 / 2s)$			
$(v = impact \ velocity; \ s =$	 dynamic compression dia 72.1 m/s² 	<i>sctance):</i> 78.7 m/s ²	78.7 m/s ²

*) Not recorded owing to minor changes in design of the RIMOB in comparison with test F7. The calculation of the 'average acceleration' (see below) shows that the level of acceleration of tests F11 and F13 is slightly higher than that of test F7.



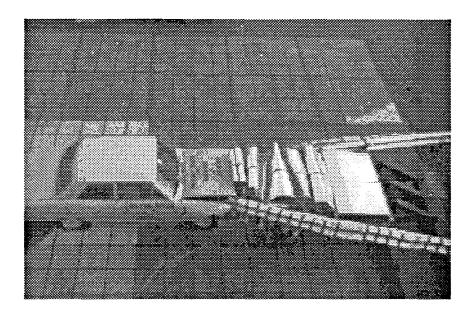


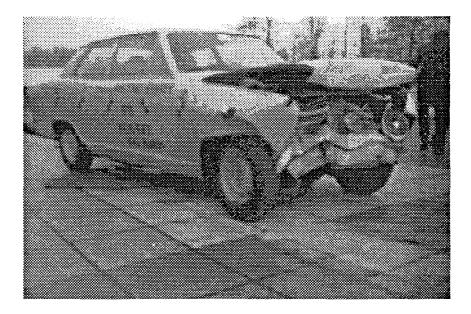


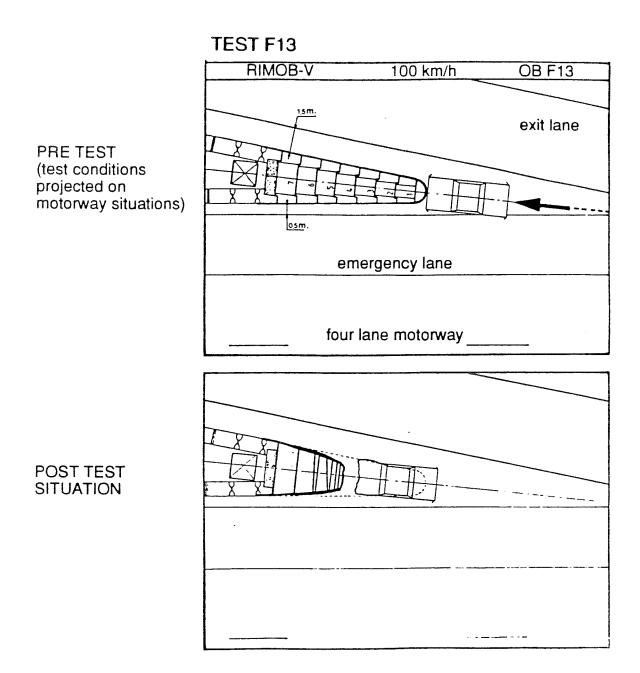


Vehicle deceleration not recorded

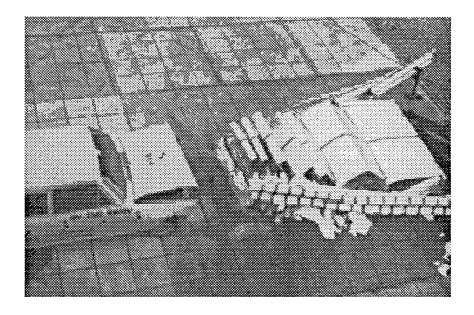
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Vehicle deceleration not recorded





5.2. Offset tests

D. CEN test specifications TC 2.1.B.

Target impact speed:	80 km/h
Target impact angle:	0°
Target impact point:	center 1/4 offset
Target vehicle test mass:	900 kg

E. Test performed

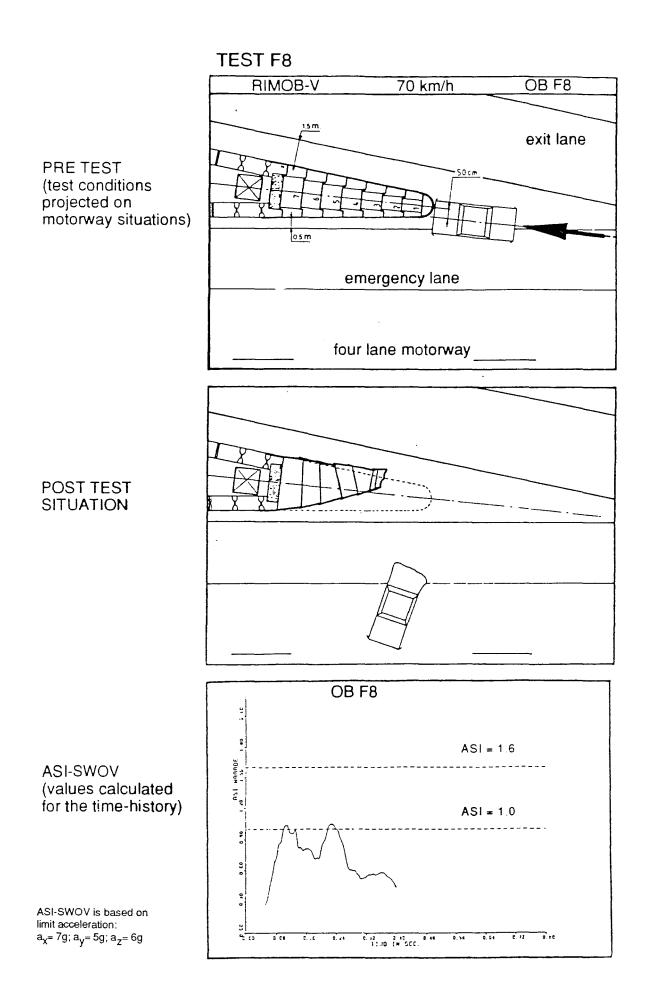
Two tests are carried o	ut: Test-number	F8	
Test impact speed:	70 km/h	(12.5% difference)	
Test impact angle:	0°	(0% difference)	
Test impact point:	0.5 m from the	right side of the car's c	enter
and Test-number F12			
Test impact speed:	80 km/h	(0% difference)	
Test impact angle:	0°	(0% difference)	
Test impact point:	0.5 m from the	right side of the car's c	enter
Test-number:			
	F8		F12
Car:			
	Opel Kadett I	В	Opel Kadett B
Model year:	10(0		1071
	1969		1971
Test mass:			
1 COT 114405.	970 kg		955 kg
	e		-
Test date:			
	08.26.81		11.18.81

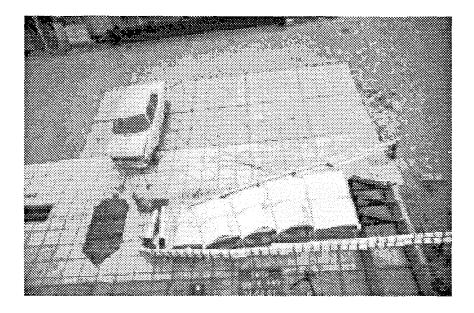
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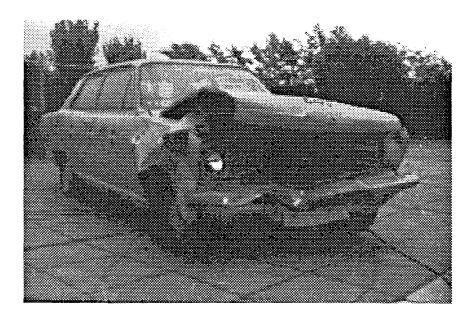
F. Results TC 2.1.B.

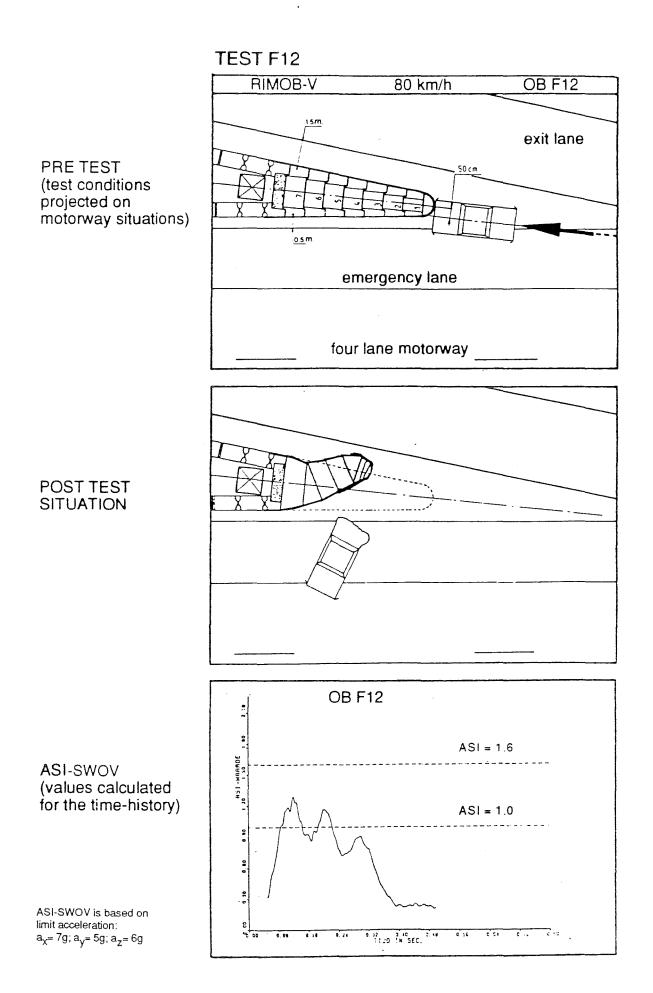
F.1. Data of the RIMOB

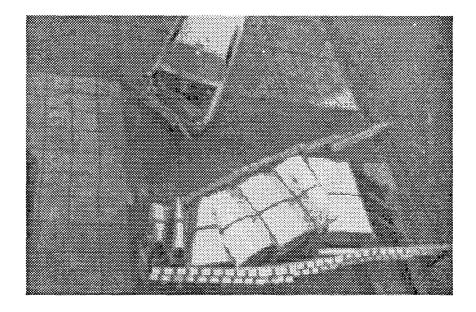
Test-number:	F8	F12
Damage to RIMOB:	compression: 2.4 m	compression: 3.3 m
Maximum permanent d	eflection (lateral): 0.33 m	0.95 m
Major parts fractured o	or detached?: none	none
F.2. Vehicle		
Rebound:	3 m	1.5 m
Length reduction of ho	<i>od:</i> 0.34 m	0.37 m
Vehicle cockpit deform	ation index VCDI: RF 0 0 0 0 0 0 0 floor intrusion of 3 cm	RF 0 0 1 0 0 0 0 0 floor intrusion of 6 cm
F.3. Injury assessmen	t	
Acceleration severity in (criteria: ASI _{max-belted} =	<i>1,0)</i> : 0.63	0.76
	adex ASI-SWOV (zie graphs) 1,6; ASI _{max-unbelted} = 1,0;) 1.1	1.3
HIC value: (criteria: max = 1000)	not registered	driver: 98 passenger: 93
Maximum shoulder bela (a general accepted cri		driver: 3091 N passenger: 5144 N

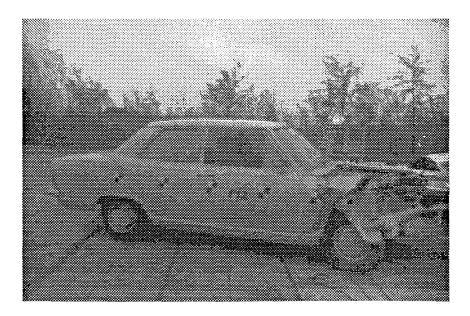












5.3. Frontal test

G. CEN test specifications TC 3.2.B.

Target impact speed:	80 km/h
Target impact angle:	15°
Target impact point:	nose center at 15°
Target vehicle test mass:	900 kg

H. Test performed

One test is carried out: Test impact speed: Test impact angle: Test impact point:	Test-number: F 80 km/h 15.2° nose center	(0% diff	Ference) ifference)
Test-number:			F5
Car:			Opel Kadett B
Model year:			1970
Test mass:			910 kg
Test date:			05.27.81

J. Results TC 3.2.B.

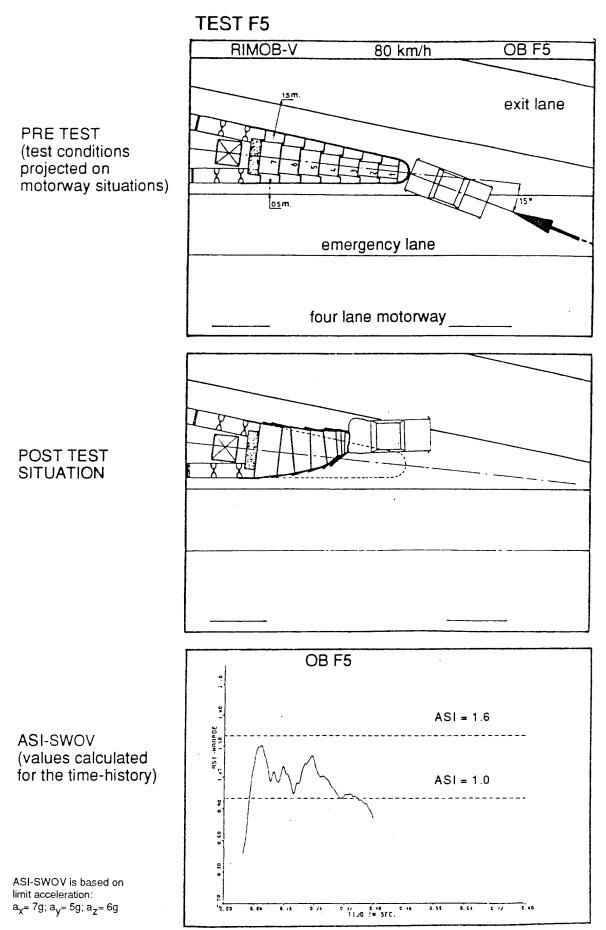
J.1. Data of the RIMOB

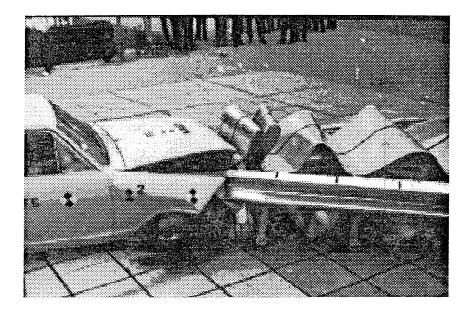
Test-number:	F5
Damage to RIMOB:	compression: 3.2 m
Maximum permanent deflection (lateral):	0.81 m
Major parts fractured or detached?:	
	none
J.2. Vehicle	
Rebound:	0.42 m
Length reduction of hood:	0.30 m
Vehicle cockpit deformation index VCDI:	no deformation
J.3. Injury assessment	
Acceleration severity index ASI-CEN: (criteria: $ASI_{max-belted} = 1,0$):	0.99

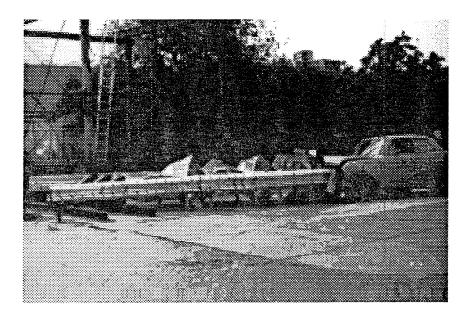
Acceleration severity index ASI-SWOV (zie graphs) (criteria: $ASI_{max-belted} = 1,6$; $ASI_{max-unbelted} = 1,0$;)

1.5

0.88







5.4. Side impact test 65 km/h, 22°

K. CEN test specifications TC 4.2.A.

Target impact speed:	50 km/h
Target impact angle:	15°
Target impact point:	side impact (middle of construction)
Target vehicle test mass:	1300 kg

L. Test performed

One test is carried out: Test impact speed: Test impact angle: Test impact point:	65 km/h 22.4°	(30% di (49.3%	fference) difference)
Test-number:			F4
Car:			Opel Kadett B
Model year:			1971
Test mass:			910 kg
Test date:			05.27.81

M. Results TC 4.2.A.

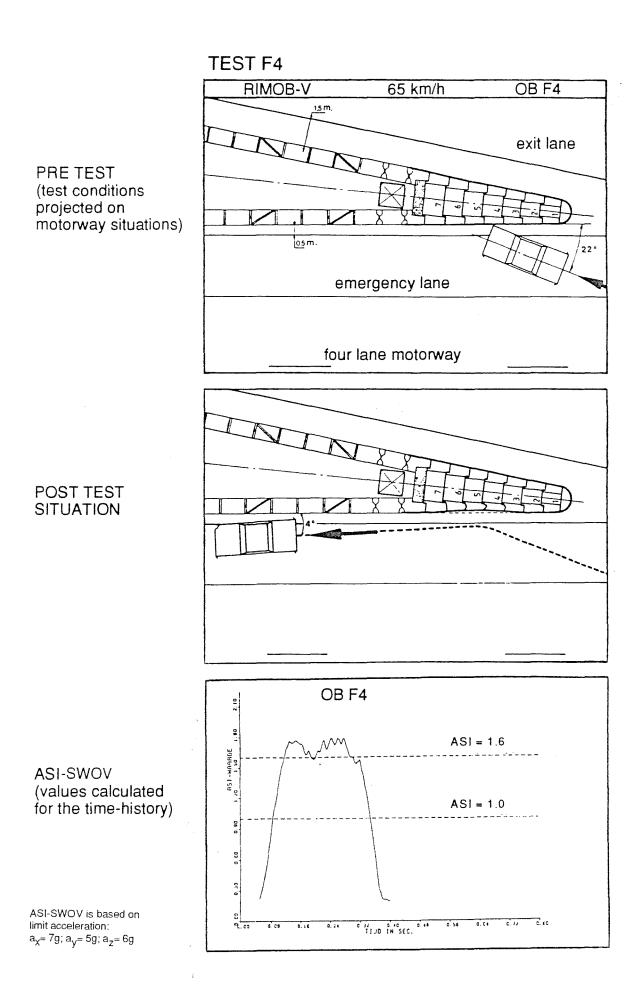
M.1. Data of the RIMOB

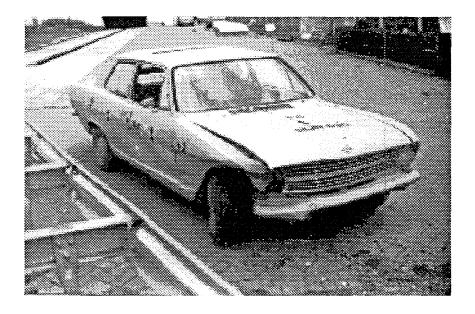
Test-number:	F4
Damage to RIMOB:	One tube has been slightly deformed
Maximum permanent deflection (lateral):	0.10 m (departure side)
Major parts fractured or detached?:	none
M.2. Vehicle	
Rebound:	not applicable
Exit angle:	4° to guard rail
Vehicle damage:	small dents and scratches
Vehicle cockpit deformation index VCDI:	no deformation

M.3. Injury assessment

Acceleration severity index ASI: (criteria: $ASI_{max-belted} = 1,0$) Acceleration severity index ASI-SWOV (zie graphs): (criteria: $ASI_{max-belted} = 1,6$; $ASI_{max-unbelted} = 1,0$;) 1.8 *)

*) ASI is not fully appropriate for side impact tests. See for instance the data of the head acceleration of the instrumented dummies at the side impact test F10. The values show a HIC-value which is far below the criteria of 1000.







5.5. Side impact tests 80 km/h, 15°

N. CEN test specifications TC 4. 2. B.

Target impact speed:	80 km/h
Target impact angle:	15°
Target impact point:	side impact (middle of construction)
Target vehicle test mass:	1300 kg

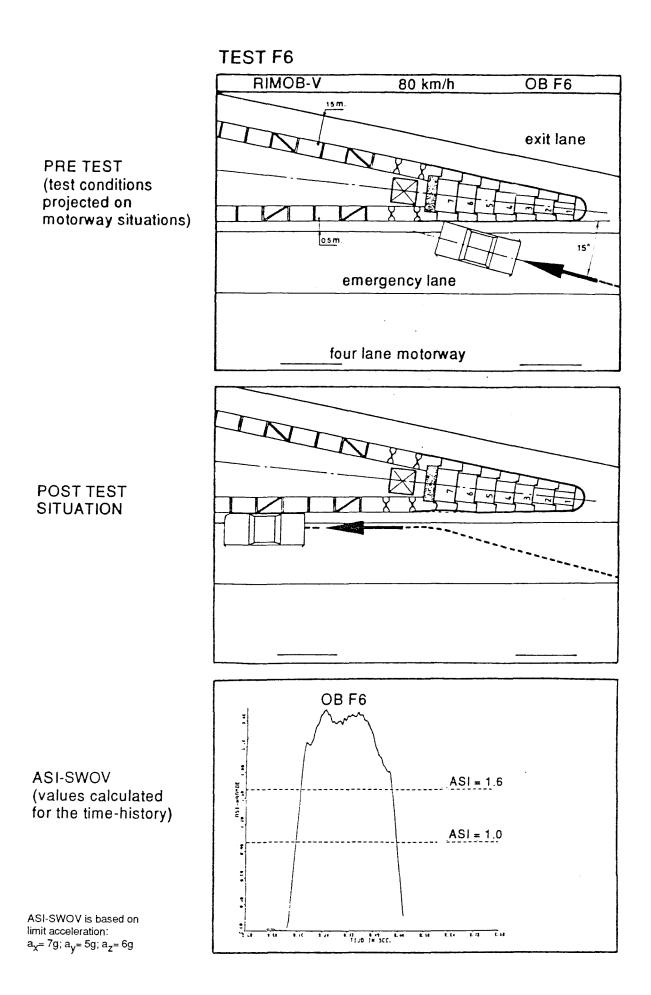
O. Test performed

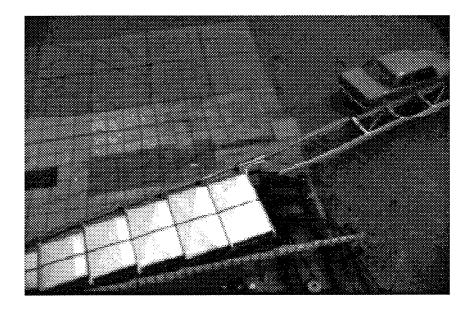
Two tests are carried of Test impact speed: Test impact angle: Test impact point:	out: Test-number 80 km/h 15° side (near back	(0% difference) (0% difference)	
Test-number	F6		F10
Car:	Opel Kadett	В	Opel Kadett B
Model year:	1972		1972
Test mass:	905 kg		965 kg
Test date:	06.24.81		11.17.81

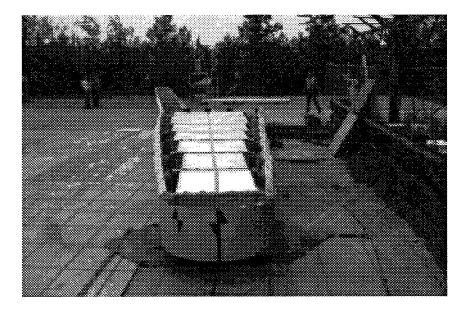
P. Results TC 4.2.B.

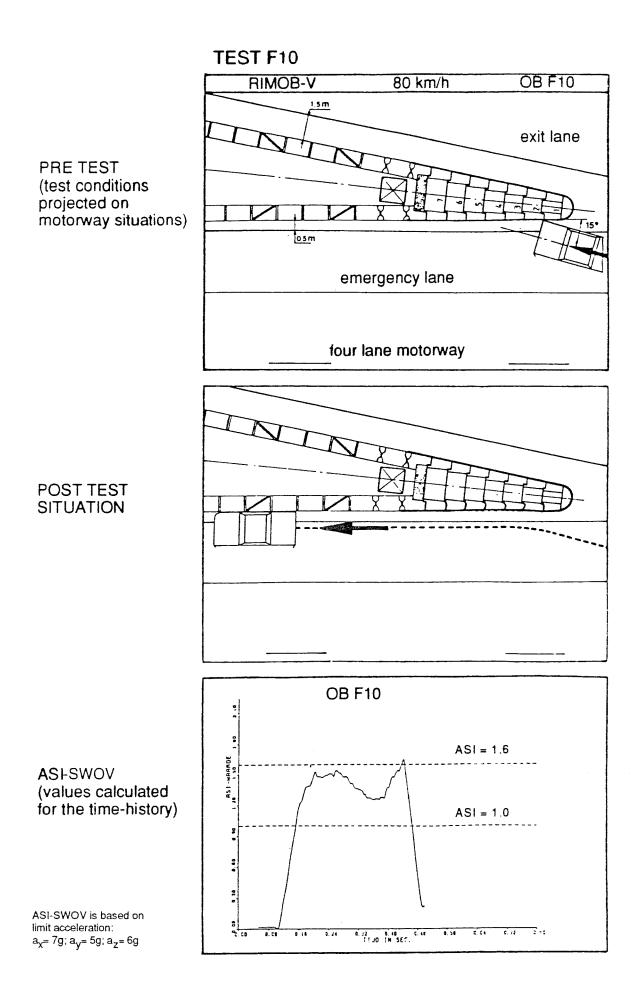
P.1. Test item		
Test-number	F6	F10
Damage to RIMOB:	slight	slight
Maximum permanent de	flection (lateral): 0 m (departure side)	0.25 m (departure side)
Major parts fractured of	r <i>detached?:</i> none	none
P.2. Vehicle		
Rebound:	not applicable	not applicable
Exit angle:	0° to guard rail	0° to guard rail
Vehicle damage:	small dents and scratches	small dents and scratches
Vehicle cockpit deforma	tion index VCDI: no deformation	no deformation
P.3. Injury assessment		
Acceleration severity ind (criteria: $ASI_{max-belted} = 1$)		1.03 *)
Acceleration severity ind (criteria: $ASI_{max-belted} = 1$)	lex ASI-SWOV (zie graphs) ,6; ASI _{max-unbelted} = 1,0;) 2.5 *)	1.6 *)
HIC: (criteria: max = 1000)	not registered	95
Maximum shoulder belt (a general accepted crite		2000 N

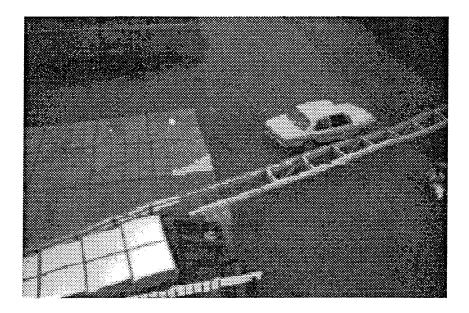
*) ASI is not fully appropriate for side impact tests. See the results of the instrumented dummy at test F10. The values of the ASI are rather high, while the values of the head acceleration and belt load are low.

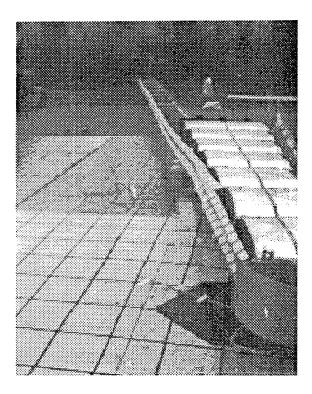












5.5. RIMOB-P, frontal test

Q. CEN test specifications TC 1. 1. B.

Not applicable: RIMOB-P is developped for a collision speed up to 70 km/h.

R. Test performed

One test is carried out: Test impact speed: Test impact angle: Test impact point:	Test-number: F 70 km/h 0° center	9 (12.5% difference) (0% difference)
Test-number:		F9
Car:		Opel Kadett B
Model year:		1973
Test mass:		946 kg
Test date:		08.26.81

S. Results TC 1. 1. B.

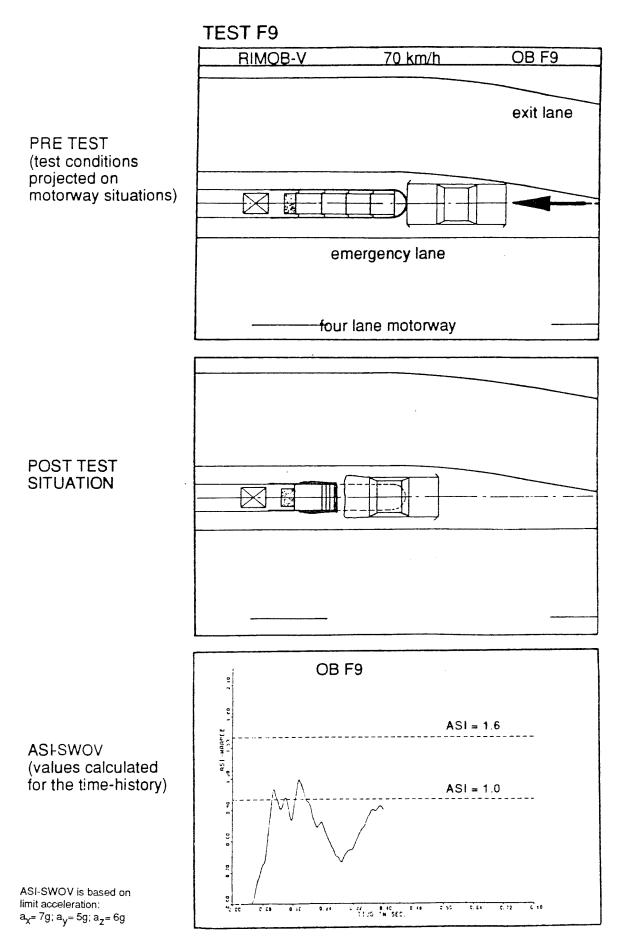
S.1. Data of the RIMOB

Test-number:	F9
Damage to RIMOB:	compression: 2.9 m dynamic compression: 2,9 m
Maximum permanent deflection (lateral):	0 m
Major parts fractured or detached?:	none
S.2. Vehicle	
Rebound:	0.26 m
Length reduction of hood:	0.21 m
Vehicle cockpit deformation index VCDI:	no deformation
S.3. Injury assessment	
Acceleration severity index ASI: (criteria: $ASI_{max-belled} = 1,0$):	0.71

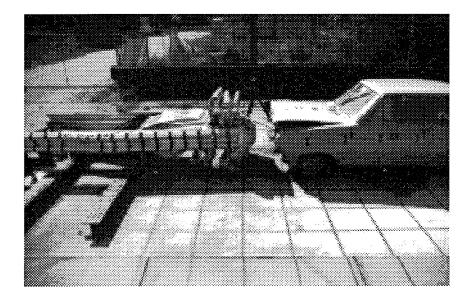
0.71

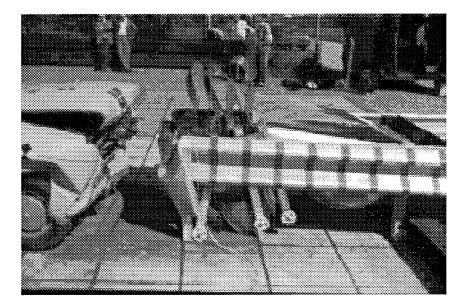
Acceleration severity index ASI-SWOV (zie graphs) (criteria: $ASI_{max-belted} = 1,6$; $ASI_{max-unbelted} = 1,0$;) 1.2

Average acceleration $(a_{avg.} = v^2 / 2s)$ (v = impact velocity; s = dynamic compression disctance): 65,2 m/s²



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6. Final results

Crash cushion behaviour

No elements of the crash cushion penetrate the passenger compartment of the vehicle. No major pars of the crash cushion becomes totally detached. Anchorages and fixings perform to the design specifications.

Vehicle behaviour

The vehicle remains upright during and after the collision

Summary of impact test acceptance criteria

In the next table a summary is given in the way the RIMOB meets the acceptance criteria. It is in accordance with the classes mentioned in the CEN standard.

The classes A (ASI), W1 (redirection) and D1 (deflection) represent an acceptance on the highest level. Classes B (ASI), W2 (redirection) and D2 (deflection) represent a lower level.

A - - A A	W1 W1 W1 W2 W1	D1 D1 D1 D1 D1 D1
- A	W1 W1 W2	D1 D1 D1
A	W1 W1 W2	D1 D1 D1
	W1 W2	D1 D1
	·· -	וע
4	W1	D1
3*	W1	D1
3*	W1	D1
4/B*	W1	D1
A	W1	D1
	3* 3* 4/B*	B* W1 B* W1 A/B* W1

*) ASI is not fully appropriate for side impact tests. See the remarks at side impact test F10

Concluded is that the RIMOB meets fully the highest class D. With the exception of the results of one test (F8), the Rimob meets also the highest class W. Concerning the acceptance criteria for the ASI, the RIMOB meets the highest class A for the frontal tests. Concerning the side impact tests a remark is given below the table.

This leads to the final conclusion that the RIMOB V-shape is a safe construction for application as crash cushion on motorways.

7. General statements

The test results in this report relates only to the items tested.

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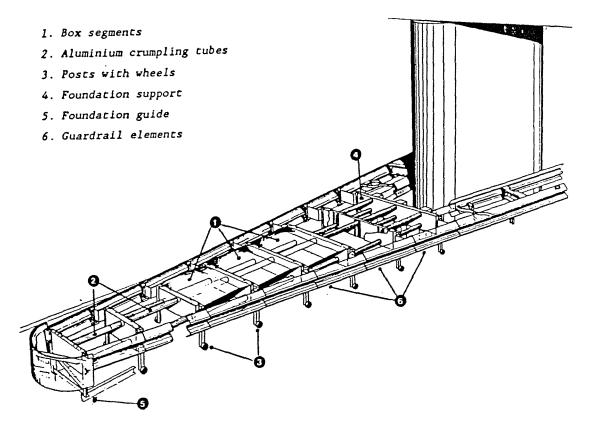
8. Approval of report

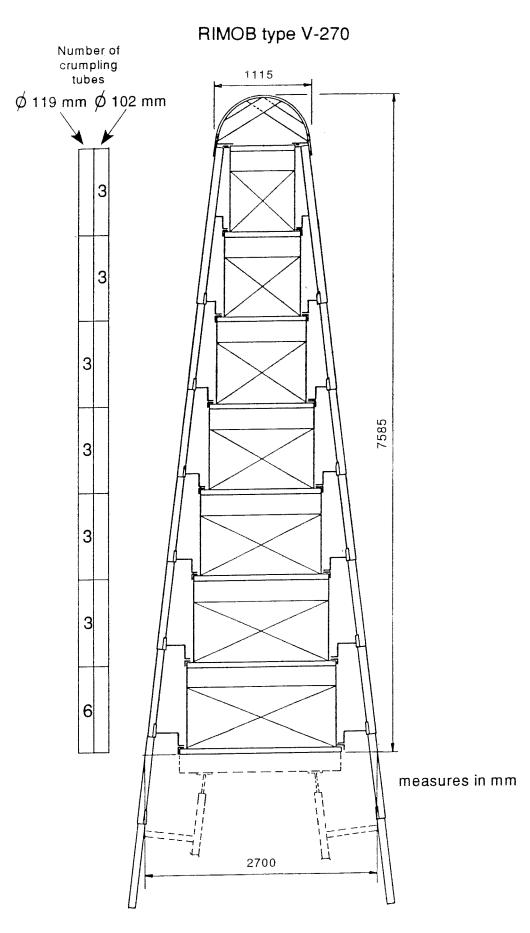
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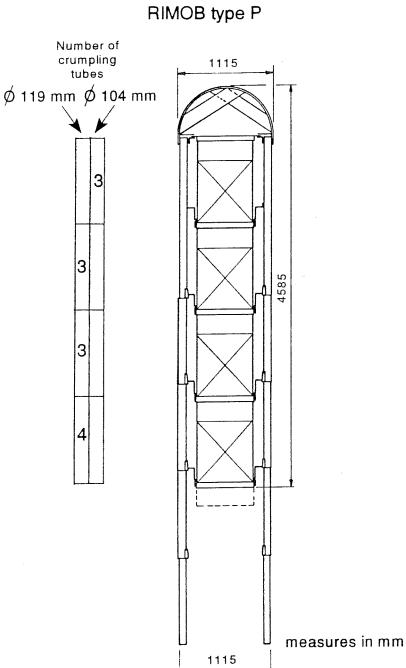
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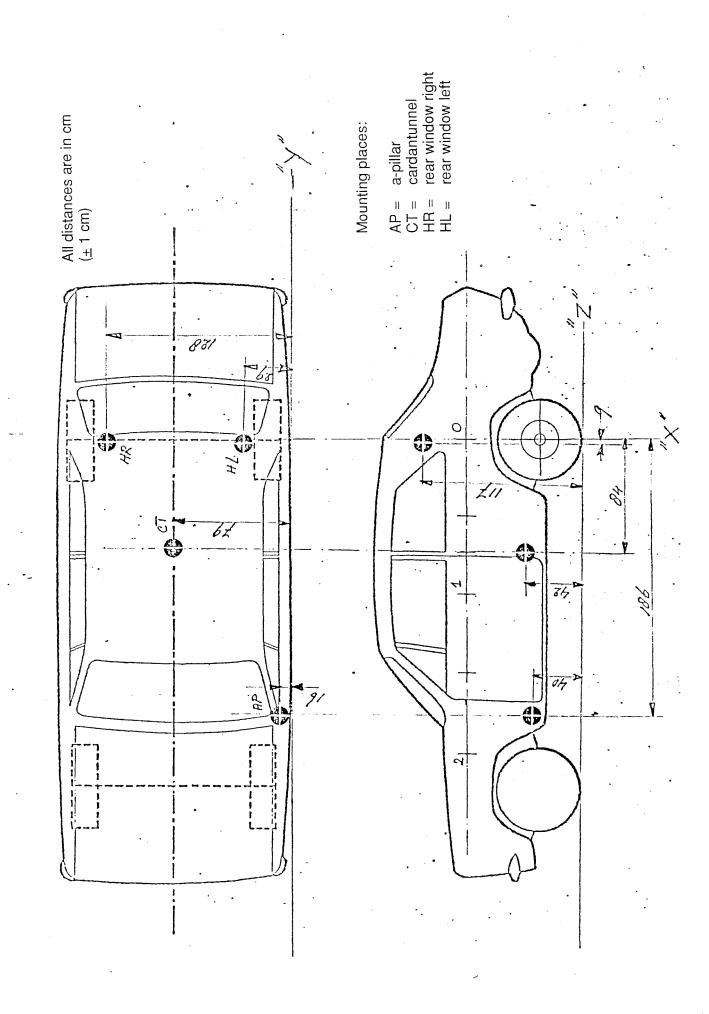
Title:

Open-worked drawing of RIMOB









ANNEX 4